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TITLE OF THE INVENTION

MOTOR-DRIVEN POWER STEERING APPARATUS

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CROSS-REFERENCE TO PRIOR APPLICATION

This is a U.S. National Phase Application under 35 U.S.C.
§371 of International Patent Application No. PCT/JP2004/017790
filed November 30, 2004, and claims the benefit of Japanese Patent
10 Application No. 2003-409449 filed December 8, 2003 both of which
are incorporated by reference herein. The International
Application was published in Japanese on June 23, 2005 as WO
2005/056367 A1 under PCT Article 21(2).

15 TECHNICAL FIELD

The present invention relates to a motor-driven power
steering apparatus transmitting a rotating torque of an electric
motor to a steering shaft by a drive gear provided in an output shaft
of the electric motor and a driven gear provided in the steering
20 shaft.

BACKGROUND ART

In a steering apparatus for a motor vehicle in recent days, a
motor-driven power steering apparatus making good use of an

electric motor is well employed as a steering assist mechanism.

The motor-driven power steering apparatus transmits a rotating torque of the electric motor to a steering shaft via a worm gear.

However, in the worm gear, since a transmission efficiency of

- 5 the rotating torque is comparatively low such as 60 to 80 %, in the case that a speed reduction ratio is set constant, an electric motor having a larger output torque is necessary for transmitting a predetermined rotating torque. Accordingly, there is a problem that an outer diameter of the electric motor becomes large and it is
10 hard to make an entire of the steering apparatus compact.

- Therefore, there has been designed a speed reducer in which the output shaft of the electric motor is attached in such a manner as to be in almost parallel to the steering shaft, and which uses a spur gear or a helical gear in which the transmission efficiency of the
15 rotating torque is comparatively high.

- In the case of using the spur gear or the helical gear for the speed reducer, the transmission efficiency of the rotating torque becomes comparatively high such as about 95 %. Accordingly, it is possible to reduce the output torque of the electric motor at that
20 degree, and it is possible to make the entire of the steering apparatus compact by suppressing an enlargement of an outer shape of the electric motor.

- However, in the case of employing the speed reducer, for example, using the spur gear, if it is intended to obtain a necessary
25 speed reduction ratio on the basis of a one-stage structure of the

gear provided in the output shaft of the electric motor, and the gear attached to the steering shaft engaging with the gear, a pitch circle of the steering shaft side gear becomes large, and it is impossible to improve the condition that it is hard to intend to make the entire of the steering apparatus compact.

On the other hand, in the case of employing a speed reducer having a multi-stage structure, for example, having intermediate gears, in place of the speed reducer having the one-stage structure, as the speed reducer using the spur gear, it is possible to intend to make the entire of the steering apparatus compact, however, there is generated a new problem that a comfortable steering feeling is reduced due to an increase of a backlash, a cost increase due to a complication of the structure of the speed reducer or the like.

In order to solve the problem mentioned above, for example, Japanese Patent Application Laid-Open No. 11-124045 discloses a motor-driven power steering apparatus in which an entire of a steering apparatus having an electric motor and a speed reducer arranged therein can be made compact by accommodating a speed reducer constituted by a pair of spur gears or helical gears having a high speed reduction ratio within a housing, and arranging the electric motor close to the housing in which a steering shaft is accommodated.

In the motor-driven power steering apparatus disclosed in the Japanese Patent Application Laid-Open No. 11-124045, since it is hard to secure a strength of the gear on the basis of a normal

involute tooth profile, a strength of a tooth surface is secured by employing a tooth profile based on a predetermined special theory.

DISCLOSURE OF THE INVENTION

5 Problem to be Solved by the Invention

However, it is hard in structure to actually manufacture the tooth profile based on the special theory disclosed in the Japanese Patent Application Laid-Open No. 11-124045, and there comes into question whether or not it is possible to stably supply a speed
10 reducer having a high quality in a mass production line. In other words, since there is employed the tooth profile based on the special theory, a performance of the speed reducer tends to be strongly affected by an alignment error of the gear. Accordingly, a high processing precision and a high assembling precision are required
15 in the mass production line. Further, there are a lot of problems remaining for being actually changed to the mass production line, such as it is impossible to process by an existing manufacturing equipment, an inspection method of the processing precision is not established, and the like.

20 The present invention is made by taking the circumstance mentioned above into consideration, and an object of the present invention is to provide a motor-driven power steering apparatus which can achieve a predetermined speed reduction ratio even in the case that the motor-driven power steering apparatus is
25 constituted by a pair of spur gears or helical gears, and can secure a

sufficient gear strength on the basis of a simple structure.

Means for Solving the Problem

In order to achieve the object mentioned above, in accordance
5 with a first aspect of the present invention, there is provided a
motor-driven power steering apparatus in which a rotating torque of
an electric motor is transmitted to a steering shaft by a drive gear
provided in an output shaft of the electric motor and a driven gear
provided in the steering shaft, and a speed reduction ratio is equal
10 to or more than 3, wherein the steering shaft and the output shaft
of the electric motor are arranged in almost parallel, a center
distance between both the shafts is equal to or more than 35 mm
and equal to or less than 90 mm, and the drive gear is configured
such that a number of teeth is equal to or more than 6 and equal to
15 or less than 15, a module is equal to or more than 0.8 and equal to
or less than 1.5, a tooth depth is equal to or less than 2.4 times of
the module, and a pressure angle is equal to or more than 14.5
degrees and equal to or less than 30 degrees, and a torsion angle is
equal to or more than 0 degrees and equal to or less than 40
20 degrees.

In the motor-driven power steering apparatus in accordance
with the first aspect of the present invention, since there is
employed a pair of gears in which steering shaft and the output
shaft of the electric motor are in almost parallel, a transmission
25 efficiency of the rotating torque is high, and it is possible to arrange

the entire of steering apparatus compact. Further, on the basis of the data dimensions mentioned above, even in the case of using the gear which can be manufactured in the normal manufacturing step without using the tooth profile based on the predetermined special
5 theory, it is possible to secure correct values of a trochoid interference clearance, a tooth thickness of a tooth top and a tooth surface stress.

Further, in accordance with a second aspect of the present invention, there is provided a motor-driven power steering
10 apparatus as recited in the first aspect, wherein an involute gear in which a tooth profile is configured in such a manner that a pressure angle is increased from a tooth top of the gear to a tooth root is employed for one or both of the drive gear and the driven gear.

In the motor-driven power steering apparatus in accordance
15 with the second aspect of the present invention, it is possible to reduce a tooth root stress at a time when a maximum torque is applied, by employing the involute gear in which the tooth profile is formed in such a manner that the pressure angle is increased from the tooth top of the gear to the tooth root, and it is possible to secure
20 a durability of the gear.

Further, in accordance with a third aspect of the present invention, there is provided a motor-driven power steering apparatus as recited in the first or second aspect, wherein an involute gear in which a crowning process is applied in a direction of
25 a tooth trace is employed for one or both of the drive gear and the

driven gear.

In the motor-driven power steering apparatus in accordance with the third aspect of the present invention, since the involute gear in which the crowning process is applied in the direction of the tooth trace is employed, the tooth surface stress can be reduced. Accordingly, even in the case that a continuous operation is executed under a rated load condition, it is possible to secure a durability of the gear.

10 Effect of the Invention

In accordance with the present invention, since there is employed a pair of gears in which the steering shaft and the output shaft of the electric motor are in almost parallel, it is possible to obtain the motor-driven power steering apparatus in which the transmission efficiency of the rotating torque is high, and which is arranged compact as a whole. Further, on the basis of the data dimensions mentioned above, it is possible to secure the correct values of the trochoid interference clearance, the tooth thickness of the tooth top and the tooth surface stress, without employing the tooth profile based on the predetermined special theory.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a cross sectional view showing a schematic structure of a motor-driven power steering apparatus in accordance with an embodiment of the present invention:

FIG. 2 is a view showing a relation between a number of teeth of a small gear and a module of the small gear;

FIG. 3 is a view showing a relation among a pressure angle, a trochoid interference clearance of the small gear, and a tooth
5 thickness of a tooth top;

FIG. 4 is a view showing a relation between a tooth surface stress with respect to a tooth depth of the small gear and a tooth thickness of the tooth top; and

FIG. 5 is an explanatory view of a tooth surface shape of a
10 speed reducer used in the motor-driven power steering apparatus in accordance with the embodiment of the present invention.

Description of Reference Numerals

| | | |
|----|----------|--------------------------|
| | 1 | speed reducer |
| 15 | 5 | large gear (driven gear) |
| | 6 | small gear (drive gear) |
| | 7 | electric motor |
| | h | tooth depth |
| | m | module |
| 20 | L | center distance |
| | Z | number of teeth |
| | α | pressure angle |

BEST MODE FOR CARRYING OUT THE INVENTION

25 FIG. 1 is a cross sectional view showing a schematic

structure of a motor-driven power steering apparatus in accordance with an embodiment of the present invention. As shown in FIG. 1, the structure is made such that a steering torque acting on a steering member 4 is transmitted to a steered wheel side via a steering shaft constituted by an input shaft 12, a torsion bar 13 and an output shaft 14, and a rotating torque of an electric motor 7 is transmitted to the steered wheel side via a speed reducer 1 constituted by a small gear (a drive gear) 6 and a large gear (a driven gear) 5, and the output shaft 14 of the steering shaft.

10 The input shaft 12 is coupled to the steering member 4, and corresponds to one constituting element of a torque transmission means for transmitting the steering torque acting on the steering member 4 to the steered wheel side. The input shaft 12 is configured such that one end side is supported via a bearing (not shown), and the other end side is coupled to the torsion bar 13.

15 The torsion bar 13 couples the input shaft 12 and the output shaft 14, and generates a torsional deformation on the basis of the steering torque, thereby generating a relative displacement of rotating angle between the input shaft 12 and the output shaft 14.

20 The output shaft 14 is configured such that one end side is supported via bearings 11, 11, ..., and the other end side is coupled to the torsion bar 13. The output shaft 14 transmits the steering torque from the torsion bar 13 to the steered wheel side, and transmits the rotating torque of the electric motor 7 transmitted from the speed reducer 1 to the steered wheel side. Accordingly,

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the input shaft 12 and the output shaft 14 are elastically and relatively rotated in correspondence to the steering torque and are coaxially coupled.

A torque detecting mechanism 15 is configured such as to
5 detect the relative displacement of rotating angle between the output shaft 14 and the input shaft 12 generated due to the torsion of the torsion bar 13 by the steering torque, thereby detecting the steering torque.

The speed reducer 1 is configured by a spur gear or a helical
10 gear which is provided with the large gear 5 provided in the output shaft 14 of the steering shaft, and the small gear 6 provided in the output shaft of the electric motor 7. It is possible to arrange the electric motor 7 in almost parallel to the steering shaft, by employing the spur gear or the helical gear. However, a physical
15 restriction on a layout is generated in an outside dimension of the electric motor 7 in correspondence to a center distance L between the steering shaft and the output shaft of the electric motor 7. For example, in the case that the maximum allowable outside dimension of the electric motor 7 is constituted by a diameter 73
20 mm and a height 95 mm, on the basis of the restriction on the layout, in order to secure a rotating torque equal to or more than 35 Nm for a steering assist torque around the steering shaft, a rating torque is set to 4 Nm, the center distance L is set to 55 mm, and a speed reduction ratio is set to about 10.

25 FIG. 2 is a view showing a relation between a number of

teeth Z of the small gear 6 and a module m of the small gear 6 in the case that the center distance L between the steering shaft and the output shaft of the electric motor 7 is set to 55 mm, the speed reduction ratio is set to 10, and a torsion angle β is set to 25 degrees.

5 A diameter $d (= Z \times m)$ of a pitch circle of the small gear 6 is about 8 to 10 mm, however, in order to avoid a condition that the number of teeth is extremely large or extremely small, a practical range exists in the number of teeth Z equal to or more than 6 and equal to or less than 15, and the module m equal to or more than 0.8 and equal to

10 or less than 1.5.

Next, taking into consideration a manufacturing error of the gear, and an elastic deformation of the tooth of the gear in the case of executing the rated load operation, a pressure angle α setting a trochoid interference clearance and a tooth thickness of a tooth top

15 to correct values is selected. FIG. 3 is a view showing a relation among the pressure angle α of the small gear 6, the trochoid interference clearance and the tooth width of the tooth top in the case that the number of teeth Z is 10, the module m is 0.95 and a tooth depth h is 2.25 times of the module m . In FIG. 3, a circle

20 mark indicates a trochoid interference clearance, and a rectangle mark indicates a value obtained by dividing the tooth thickness of the tooth top by the module value, respectively.

In order to avoid the trochoid interference from being generated, the trochoid interference clearance equal to or more than

25 0.2 mm is necessary. As shown in FIG. 3, in the case that the

- pressure angle α is equal to or more than 14.5 degrees and equal to
ore less than 35 degrees which is defined as a standard value in
Japanese Industrial Standards (JIS), the trochoid interference
clearance becomes equal to or more than 0.2 mm in a region where
- 5 the pressure angle α is equal to or more than 23 degrees.
- Accordingly, the trochoid interference is not generated. On the
other hand, in order to secure a tooth top strength, the tooth
thickness of the tooth top equal to or more than 0.3 times of the
module m is necessary. As shown in FIG. 3, in order to secure the
- 10 tooth thickness of the tooth top equal to or more than 0.3 times of
the module m , it is necessary to set the pressure angle α to be equal
to or less than 27 degrees. In this case, the practical range exists
in the torsion angle β equal to or more than 0 degrees and equal to
or less than 40 degrees.
- 15 Further, in the case that a steel material is employed as a
material of the small gear 6 and the large gear 5, it is possible to
approximately determine a tooth surface stress σ_H with respect to a
tangential load P_n in a perpendicular direction to the tooth of the
small gear 6 generated on the basis of an auxiliary rotating torque
- 20 by using (numerical expression 1).

[numerical expression 1]

$$\sigma_H = \sqrt{0.35 \cdot E \cdot P_n \left[\frac{Z_1 + Z_2}{Z_2} \right] \frac{\cos^2 \beta_g}{N_b \cdot \varepsilon_s \cdot b \cdot d_b \cdot \sin \alpha_b}}$$

In this case, in (numeral expression 1), reference symbol E denotes a longitudinal elastic modulus of a material (a steel material in the present embodiment) of the gear, reference symbol ε_s denotes a front surface contact ratio, reference symbol b denotes a
5 tooth width of the small gear 6, reference symbol d_b denotes a mating pitch circle diameter of the small gear 6, reference symbol α_b denotes a mating pressure angle of the small gear 6, reference symbol β_g denotes a torsion angle of a base cylinder of the small gear 6, reference symbol Z_1 denotes a number of teeth of the small
10 gear 6, reference symbol Z_2 denotes a number of teeth of the large gear 5, and reference symbol N_b denotes an availability of the tooth width, respectively.

FIG. 4 is a view showing a relation of the tooth surface stress σ_s and the tooth thickness of the tooth top with respect to the tooth
15 depth h of the small gear 6, in the case of setting E to 206000 N/mm², P_n to 946, N_b to 14 mm, Z_1 to 10, Z_2 to 97, m to 0.95, the pressure angle α to 25 degrees, the torsion angle β to 25 degrees, d_b to 10.308 mm, α_b to 25.283 degrees, β_g to 22.521 degrees, and N_b to 0.995. In FIG. 4, a circle mark indicates a tooth surface stress, and
20 a rectangle mark indicates a value obtained by dividing the tooth thickness of the tooth top by the module value, respectively.

In the case of setting a target value of the tooth surface stress σ_H to a threshold value 1760 N/m² or less on design of a power transmission system gear of a motor vehicle, and setting a
25 target value of the tooth thickness of the tooth top to 0.3 times of

the module m or more, it is possible to satisfy both the conditions in the case that the tooth depth h is set to equal to or less than 2.4 times of the module m , as is apparent from FIG. 4.

FIG. 5 is an explanatory view of a tooth surface shape of the speed reducer 1 used for the motor-driven power steering apparatus in accordance with the embodiment of the present invention. In order to compensate for the reduction of the tooth root strength, the tooth surface shape of any one of the large gear 5 and the small gear 6, or the tooth surface shapes of both of a pair of gears are formed by an aspect shown in FIG. 5. In FIG. 5, the tooth surface of the small gear 6 is shown by being divided into vertical and horizontal meshes. The tooth profile direction is provided with a negative pressure angle error in such a manner that the pressure angle of the tooth top becomes larger than the pressure angle of the tooth boot, and the tooth surface shape is formed in such a direction that the mutual mating stresses are increased, that is, such that the center portion forms convex. Further, a crowning process is applied in a tooth trace direction, and the tooth surface shape is formed such that the center portion forms convex in the tooth trace direction.

It is possible to equalize a distribution of the contact stress in the tooth surface of the small gear 6 used in the speed reducer 1 in the tooth profile direction and the tooth trace direction by employing the tooth surface shape mentioned above, and it is possible to compensate for the lack of the tooth root strength while

preventing a biased abrasion of the tooth surface, thereby contributing to an improvement of a durability.

CLAIMS

1. A motor-driven power steering apparatus in which a rotating torque of an electric motor is transmitted to a steering shaft by a drive gear provided in an output shaft of said electric motor and a driven gear provided in said steering shaft, and a speed reduction ratio is equal to or more than 3, wherein

said steering shaft and the output shaft of said electric motor are arranged in almost parallel, a center distance between both the shafts is equal to or more than 35 mm and equal to or less than 90 mm, and

said drive gear is configured such that a number of teeth is equal to or more than 6 and equal to or less than 15, a module is equal to or more than 0.8 and equal to or less than 1.5, a tooth depth is equal to or less than 2.4 times of the module, and a pressure angle is equal to or more than 14.5 degrees and equal to or less than 30 degrees, and a torsion angle is equal to or more than 0 degree and equal to or less than 40 degrees.

2. A motor-driven power steering apparatus as claimed in claim 1, wherein an involute gear in which a tooth profile is formed in such a manner that a pressure angle is increased from a tooth top of the gear to a tooth root is employed for one or both of said drive gear and said driven gear.

3. A motor-driven power steering apparatus as claimed in

claim 1, wherein an involute gear in which a crowning process is applied in a direction of a tooth trace is employed for one or both of said drive gear and said driven gear.

4. A motor-driven power steering apparatus as claimed in claim 2, wherein an involute gear in which a crowning process is applied in a direction of a tooth trace is employed for one or both of said drive gear and said driven gear.